

[Lecture 4]

Multi-phase equilibrium

Consider a macroscopic system with r chemical species; the system is in J co-existing phases. Then

$$E = \sum_{j=1}^J E^{(j)}$$

↑ ↓
 total en., en. in
 fixed phase (j)

Surface en. neglected: $\frac{E(\text{surf.})}{E(\text{bulk})} \sim \frac{N^{2/3}}{N} = N^{-\frac{1}{3}} \rightarrow 0$ as $N \rightarrow \infty$.

Similarly,

$$S = \sum_{j=1}^J S^{(j)} \quad [\text{bulk terms only}]$$

$$V = \sum_{j=1}^J V^{(j)}$$

$$n_i = \sum_{j=1}^J n_i^{(j)} \quad i = 1, \dots, r$$

Now, consider

$$\delta E = \sum_{j=1}^J [T^{(j)} \delta S^{(j)} - p^{(j)} dV^{(j)} + \sum_{i=1}^r \mu_i^{(j)} \delta n_i^{(j)}]$$

Small displacement from equil.

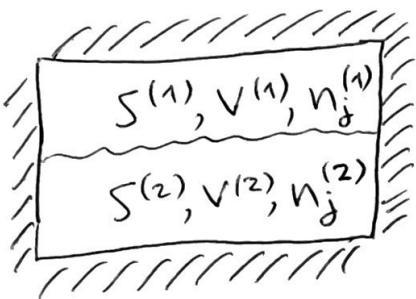
Min E principle: $(\delta E)_{S, V, n} \geq 0$
 n_1, \dots, n_r

However, total $S, V, n_i = \text{const}$:
 $i=1, \dots, r$

$$\sum_{\alpha} \delta S^{(\alpha)} = 0, \quad \sum_{\alpha} \delta V^{(\alpha)} = 0,$$

$$\sum_{\alpha} \delta n_j^{(\alpha)} = 0$$

Two-phase system ($J=2$):



$$\begin{aligned}\delta S^{(1)} &= -\delta S^{(2)}, \\ \delta V^{(1)} &= -\delta V^{(2)}, \\ \delta n_j^{(1)} &= -\delta n_j^{(2)}\end{aligned}$$

Thus,

$$0 \leq (\delta E)_{S, V, n} = (T^{(1)} - T^{(2)}) \delta S^{(1)} - (p^{(1)} - p^{(2)}) \delta V^{(1)} + \sum_{i=1}^r (\mu_i^{(1)} - \mu_i^{(2)}) \delta n_i^{(1)}.$$

Since $\delta S^{(1)}, \delta V^{(1)}, \delta n_i^{(1)}$ can be ≤ 0
 and are uncorrelated, we have:

$$\left[T^{(1)} = T^{(2)}, \quad p^{(1)} = p^{(2)}, \quad \mu_i^{(1)} = \mu_i^{(2)} \quad i=1, \dots, r \right]$$

This gives $(\delta E)_{S, V, n} = 0$

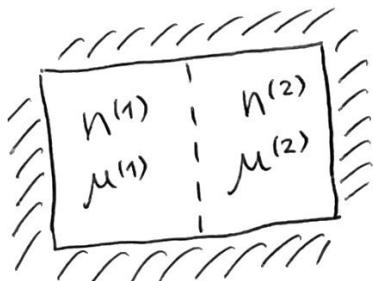
with multiple phases,

$$\left\{ \begin{array}{l} T^{(1)} = T^{(2)} = T^{(3)} = \dots \\ p^{(1)} = p^{(2)} = p^{(3)} = \dots \\ \mu_i^{(1)} = \mu_i^{(2)} = \mu_i^{(3)} = \dots \end{array} \right. \quad \begin{array}{l} \text{thermal equil.} \\ \text{mechanical " " } \\ \text{mass " " } \end{array}$$

This also means that $T, p, \mu_i = \text{const}$
in a single homogeneous phase.

Consider a composite system:

$\underbrace{r=1}_{(\text{single-species})}$



$$T^{(1)} = T^{(2)} = T$$

$$\mu^{(1)} > \mu^{(2)} \quad @ t=0$$

$$\mu_f^{(1)} = \mu_f^{(2)} \quad @ t=\infty$$

$$[\Delta n^{(1)} = -\Delta n^{(2)}]$$

$$\Delta E = T \underbrace{\Delta S}_{+} + \mu^{(1)} \Delta n^{(1)} + \mu^{(2)} \Delta n^{(2)}, \quad \text{or}$$

$$\begin{aligned} "E_f - E_i = " & \Delta S^{(1)} + \Delta S^{(2)} = \\ = 0 \text{ by construction} & = S_f - S_i \end{aligned}$$

$$\begin{aligned} \underbrace{\Delta S}_{>0} &= -\frac{\mu^{(1)}}{T} \Delta n^{(1)} - \frac{\mu^{(2)}}{T} \Delta n^{(2)} = \\ &= -\left(\frac{\mu^{(1)}}{T} - \frac{\mu^{(2)}}{T}\right) \Delta n^{(1)} \end{aligned}$$

$$\text{Thus, if } \left\{ \begin{array}{l} \mu^{(1)} > \mu^{(2)} \\ \Delta S > 0 \end{array} \right. \Rightarrow \underline{\underline{\Delta n^{(1)} < 0}}$$

matter flows
from high
 μ to low μ

In other words, $-\nabla\left(\frac{m}{T}\right)$ is a generalized force for mass flow

Likewise, we had with heat exchange:

$$\Delta S > 0 \Rightarrow \left(\frac{1}{T^{(1)}} - \frac{1}{T^{(2)}} \right) \Delta E^{(1)}_{\text{heat}} > 0$$

heat flows from ~~hot~~ to cold

Thus $-\nabla\left(\frac{1}{T}\right)$ is the generalized force for heat flow

Thermodynamic stability

$$\underbrace{(\Delta E)_{S,V,n}}_{>0} = \underbrace{(\delta E)_{S,V,n}} + (\delta^2 E)_{S,V,n} + (\delta^3 E)_{S,V,n} + \dots$$

$= 0$ @ equil.
for unconstrained systems

If $(\delta^2 E)_{S,V,n} = \begin{cases} > 0 & \text{system is stable} \\ = 0 & \text{undetermined, examine} \\ < 0 & \text{system } (\delta^3 E)_{S,V,n} \text{ is unstable} \end{cases}$

Ex.

$$\left\{ \begin{array}{l} \delta S^{(1)} + \delta S^{(2)} = \delta S = 0 \\ \delta V^{(1)} = \delta V^{(2)} = 0 \\ \delta h^{(1)} = \delta h^{(2)} = 0 \end{array} \right.$$

Then

$$\begin{aligned} \delta^2 E &= (\delta^2 E)^{(1)} + (\delta^2 E)^{(2)} = \\ &= \frac{1}{2} \left(\frac{\partial^2 E}{\partial S^2} \right)_{V,n}^{(1)} (\delta S^{(1)})^2 + \frac{1}{2} \left(\frac{\partial^2 E}{\partial S^2} \right)_{V,n}^{(2)} (\delta S^{(2)})^2 \end{aligned}$$

Recall that

$$\left(\frac{\partial^2 E}{\partial S^2}\right)_{V,n} = \left(\frac{\partial T}{\partial S}\right)_{V,n} = \frac{T}{C_V}$$

$$\textcircled{=} \frac{1}{2} (\delta S^{(1)})^2 \left[\frac{T}{C_V^{(1)}} + \frac{T}{C_V^{(2)}} \right] \geq 0, \text{ yielding } (T \geq 0)$$

$$\frac{1}{C_V^{(1)}} + \frac{1}{C_V^{(2)}} \geq 0.$$

Since the division into (1) & (2) is arbitrary, we have $\frac{1}{C_V} \geq 0 \Rightarrow C_V \geq 0$

Stable system $\Rightarrow C_V > 0$

needed to equilibrate
2 systems with $T^{(1)} \neq T^{(2)}$

Now, consider a fluctuation in $V @ T = \text{const.}$

$$\begin{cases} \delta V = \delta V^{(1)} + \delta V^{(2)} = 0, \\ \delta n^{(1)} = \delta n^{(2)} = 0 \end{cases}$$

$$(\delta^2 A)_{T,V,n} = \frac{1}{2} (\delta V^{(1)})^2 \left[\left(\frac{\partial^2 A}{\partial V^2} \right)_{T,n}^{(1)} + \left(\frac{\partial^2 A}{\partial V^2} \right)_{T,n}^{(2)} \right] \geq 0$$

Since $\left(\frac{\partial^2 A}{\partial V^2} \right)_{T,n} = - \left(\frac{\partial P}{\partial V} \right)_{T,n}$, we obtain:

$$- \left[\left(\frac{\partial P}{\partial V} \right)_{T,n}^{(1)} + \left(\frac{\partial P}{\partial V} \right)_{T,n}^{(2)} \right] \geq 0.$$

This implies $-\left(\frac{\partial p}{\partial V}\right)_{T,n} \geq 0$, or

$$K_T = -\frac{1}{V} \left(\frac{\partial V}{\partial p}\right)_{T,n} \geq 0.$$

If the equil. is stable $\Rightarrow K_T > 0$,
as $p \uparrow @ T=\text{const}, V \downarrow$.

Many other results like that
can be derived.

Phase equilibria

Suppose J phases are @ equil. at
 $T=\text{const}, p=\text{const}$. Then

$$\left[\begin{array}{l} \mu_i^{(2)}(p, T, x_1^{(2)}, \dots, x_{r-1}^{(2)}) = \\ = \mu_i^{(J)}(p, T, x_1^{(J)}, \dots, x_{r-1}^{(J)}) \end{array} \right] (*)$$

$1 \leq 2 < J \leq J$

$1 \leq i \leq r$

note that
 $\sum_{i=1}^r x_i^{(2)} = 1, \forall 2$
 mole fraction
 of species i in
 phase 2

Eq. (*) is a system of $r(J-1)$ indeps.

equations for $\underbrace{r}_{T,p} + \underbrace{J(r-1)}_{\text{mole fractions}}$ variables.

Hence, the # DoF is

$$f = \underbrace{2 + J(r-1)}_{\# \text{ vars}} - \underbrace{r(J-1)}_{\# \text{ eqs}} = 2 + r - J.$$

gibbs phase rule

Ex. $r=1$ system:

single-component
Single phase: $f = 2 + 1 - J = 2$
use P, T

can System exists anywhere in the $P-T$ plane.

Two phases:

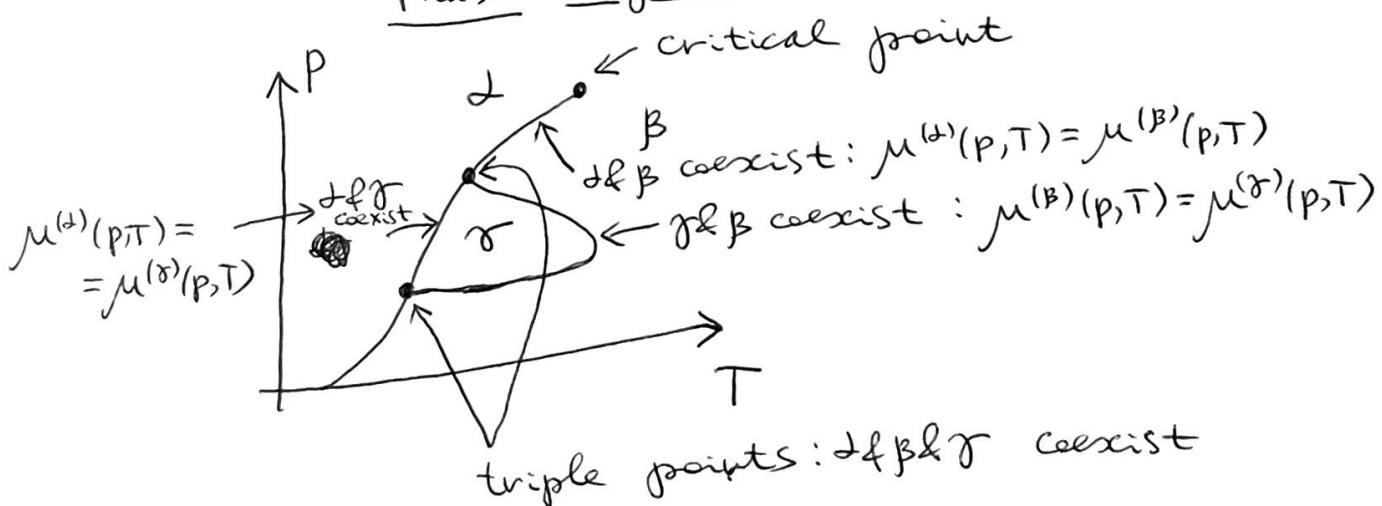
$f = 2 + 1 - 2 = 1$ \Leftarrow line in the $P-T$ plane

Three phases:

$f = 0 \Leftarrow$ 3 phases can only co-exist at a point

Cannot have > 3 phases in a single-component ($r=1$) system.

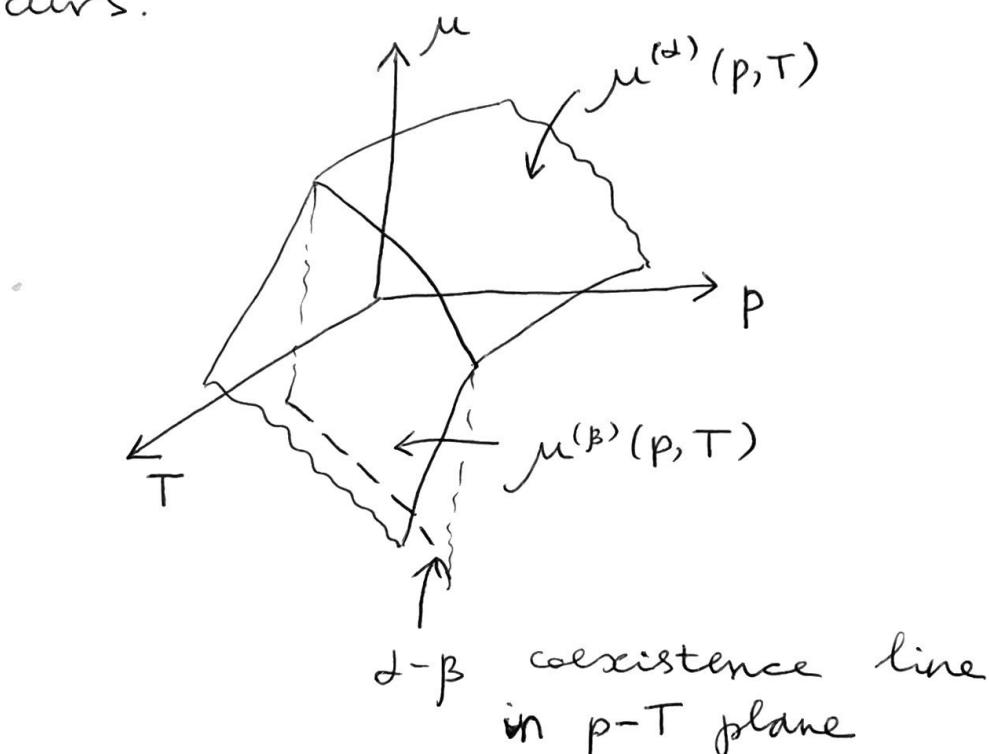
Phase diagram



For (T, p, n) variables, the relevant thermodynamic potential is Gibbs free en. G . Recall that $G = n\mu$ if $r=1$.

For phases α and β with the $\alpha-\beta$ co-existence line, the phase with the lower G (and thus μ) will be stable.

$\mu^{(\alpha)}(p, T)$ and $\mu^{(\beta)}(p, T)$ define Gibbs surfaces; the intersection of Gibbs surfaces is where a phase transition occurs.



Now, consider the Gibbs-Duhem eq'n:

$$SdT - Vdp + n d\mu = 0, \text{ or}$$

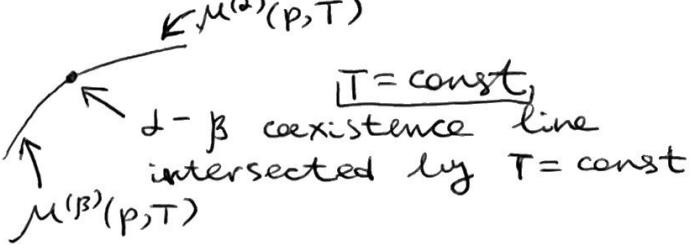
$$d\mu = \frac{V}{n} dp - \frac{S}{n} dT$$

$\underbrace{V}_{\text{volume per mole}}$ $\underbrace{S}_{\text{entropy per mole}}$

$$\text{Then } \left\{ \begin{array}{l} \left(\frac{\partial \mu}{\partial p} \right)_T = \vartheta, \\ \left(\frac{\partial \mu}{\partial T} \right)_p = -S \end{array} \right. , \quad \begin{array}{l} \text{change in } \vartheta @ T=\text{const} \\ \text{is given by a change} \\ \text{in } \left(\frac{\partial \mu}{\partial p} \right)_T \end{array}$$

Two situations:

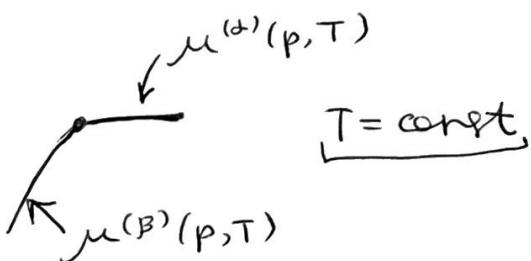
(i) no kink,
no jump in $\left(\frac{\partial \mu}{\partial p} \right)_T = \vartheta(p, T)$



Second-order, or continuous
phase transition

(ii) \exists kink where
the surfaces join:

$\vartheta(p, T)$ undergoes a
jump (i.e., $\vartheta(p, T)$ is a discontinuous
function)



First-order phase transition

Finally, consider
 $\mu^{(\alpha)}(p, T) = \mu^{(\beta)}(p, T)$ again

\downarrow
 $d\mu^{(\alpha)}(p, T) = d\mu^{(\beta)}(p, T)$ for a
small displacement along
the coexistence line

Then by GD eq'n:

$$-\dot{S}^{(\alpha)} dT + \dot{V}^{(\alpha)} dp = -\dot{S}^{(\beta)} dT + \dot{V}^{(\beta)} dp, \text{ or}$$
$$(\ast\ast) \quad \frac{dp}{dT} = \underbrace{\frac{\dot{S}^{(\alpha)} - \dot{S}^{(\beta)}}{\dot{V}^{(\alpha)} - \dot{V}^{(\beta)}}}_{\substack{\text{values for the two phases} \\ @ \text{equil. on the co-existence} \\ \text{line, with } (p, T)}} \equiv \frac{\Delta S}{\Delta V} \quad] \quad \text{Clausius-Clapeyron eq'n}$$

Note that Eq. $(\ast\ast)$ is useful only
for 1st order phase transitions \Rightarrow
 \Rightarrow RHS is ill-defined in a 2nd order
phase transition.